## LITERATURE CITED

(1) Ahrens, G.L., (to Standard Oil Development Co.), U. S. Patent 2,459,403 (Jan. 18, 1949).
(2) Am. Petrol. Inst. Research Project 44, "Selected Values of Physical and Thermodynamic Properties of Hydrocarbons and Related Compounds," Carnegie Press, Pittsburgh, 1953.
(3) Anderson, D.K., Hall, J.R., Babb, A.L., J. Phys. Chem. 62, 404 (1958)
(4) Cadogan, William, Ph.D. thesis, Massachusetts Institute of Technology, Cambridge, Mass., 1945.
(5) Chang, P., Wilke, C.R., A.I.Ch.E. Journal 1, 264 (1955).
(6) "DMF"' Product Information, Bulletin Grasselli Chemicals Department, E.I. du Pont de Nemours and Co., Wilmington, Del.
(7) Evans, T.W. (to Shell Development Co.), U. S. Patent 2,379,696 (July 3, 1945).
(8) Evans, T.W., Morris, R.C., Ibid., 2,389,144, (Nov. 20, 1945).
(9) Gerster, J.A., Gorton, J.A., Eklund, R., J. Chem. Eng. Data 5, 423 (1960).
(10) Gerster, J.A., Hill, A.B., Hochgraf, N.N., Robinson, D.G., "Tray Efficiencies in Distillation Columns," Am. Inst. Chem. Engrs., New York, 1958.
(11) Ibid., p. 2.
(12) Ibid., p. 16-18, 21-22, and Figure I-8.
(13) Ibid., p. 46 (Figure III-4)
(14) Gerster, J.A., Mizushina, T., Marks, T.N., Catanach, A.W., A.I.Ch.E. Journal 1, 536 (1955).
(15) Morris, R.C., Evans, T.W. (to Shell Development Co.), U.S. Patent 2,371,908 (Nov. 20, 1945).
(16) Patterson, J.A. (to Standard Oil Development Co.), Ibid., 2,361,493 (Oct. 31, 1944).
(17) Ibid., 2.407,977 (Sept. 24, 1946).
(18) Patterson, J.A., Sheeline, H.W., Ibid., 2,426,705 (Sept. 2, 1947).
(19) J.H. Perry, "Chemical Engineer's Handbook," 3rd ed., p. 623, McGraw-Hill, New York, 1950.
(20) Severns, W.H., Sesonske, A., Perry, R.L., Pigford, R.L., A.I.Ch.E. Journal 1, 401 (1955).
(21) Swanson, R.W., master's thesis in chemical engineering, University of Delaware, Newark, Del., June 1960.
(22) Welty, F., Gerster, J.A., Colburn, A.P., Ind. Eng. Chem. 43, 162 (1951).
(23) Wilke, C.R., Chem. Eng. Progr. 45, 218 (1949).
(24) Wohl, K., Ibid., 49, 218 (1953).

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# Saturation Properties and Liquid Compressibilities for Benzene and n-Octane 

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CCALCULATION of accurate thermodynamic properties of solutions at high temperature and pressure requires, among other things, precise knowledge of the properties of the pure components. In the course of correlating high pressure measurements on solutions that contained benzene or $n$-octane, gaps in the available liquid-phase properties and discrepancies in the vapor pressures were encountered.

The compressibilities of liquid benzene have been measured by Glanville (5) up to $237.78^{\circ}$ C.; the rapid change with temperature does not permit extrapolation of his data to higher temperatures. Compressibilities of liquid $n$-octane have been measured by Felsing (3) up to $275^{\circ} \mathrm{C}$., but the $25^{\circ} \mathrm{C}$. spacing between isotherms makes interpolation in the high-temperature region uncertain.

Numerous measurements have been made of the vapor pressure of benzene at high temperatures. Nevertheless, two recent sets of measurements ( 1,6 ) disagree by more than $1 \%$. An independent check appears necessary. The only available high-temperature vapor pressure measurements on $n$-octane date from 1900 (11)

With these deficiencies in mind, four kinds of measurements have been made on benzene and $n$-octane. These measurements, made at $10^{\circ} \mathrm{C}$. intervals, were:

|  | Temperature Range, ${ }^{\circ} \mathrm{C}$ |  |
| :--- | :--- | :--- |
| Property | Benzene | $n$-Octane |
| Vapor pressure | $130-t_{c}$ | $150-t_{c}$ |
| Saturated vapor volume | $160-280$ | $190-280$ |
| Saturated liquid volume | $130-280$ | $190-280$ |
| Liquid compressibility | $130-270$ | $130-280$ |

The saturation properties were used to derive heats of vaporization for benzene from $160^{\circ} \mathrm{C}$. to the critical temperature and for $n$-octane from $190^{\circ} \mathrm{C}$. to the critical temperature.

## EXPERIMENTAL

The benzene and $n$-octane used were American Petroleum Institute standard samples with stated purities of 99.98 and 99.94 mole $\%$. The samples arrived with magnetic break-off tips and were not exposed to air during handling. No further purification was attempted, except to remove any traces of air by distillation in vacuo. The pressure rise on going from the dew point (no liquid present) to the bubble point (no vapor present was 0.01 atm . at $200^{\circ} \mathrm{C}$.

In the experimental method (2), a sample was confined
above mercury in a calibrated glass capillary and stirred with a magnetically driven steel ball to achieve an equilibrium distribution of mercury. Volumes were determined by measuring lengths to 0.05 mm . with a cathetometer. The sample length was greater than 150 mm ., so that volume measurements should be within $0.1 \%$. Corrections were made for the effect of temperature and pressure on the capillary area. Pressures were measured with a deadweight gage; temperatures, with a platinum resistance thermometer. Critical points were determined visually.

Two sets of measurements made with different capillaries agreed within $0.1 \%$ on the average.

## VAPOR PRESSURES AND CRITICAL CONSTANTS

The measured vapor pressures can be represented by adding small corrections to the vapor pressure equations of A.P.I. Project 44 (9) that apply up to 1500 mm .:

$$
\begin{aligned}
& \text { Benzene: } \log p=4.02484-\frac{1211.033}{t+220.790}+\Delta \\
& \Delta=0, t \leqq 100^{\circ} \mathrm{C} . \\
& \Delta= \\
& n \text {-Octane: } \log p=4.511 \times 10^{-8}(t-100)^{3}, \quad 100^{\circ} \leqq t \leqq 288.84^{\circ} \mathrm{C} \\
& \begin{aligned}
\Delta= & 0, t \leqq 150^{\circ} \mathrm{C} \\
\Delta= & 0.794 \times 10^{-4}(t-150)-0.1146 \times 10^{-5}(t-150)^{2} \\
& +0.1364 \times 10^{-i}(t-150)^{3}, 150^{\circ} \leqq t \leqq 295.62^{\circ} \mathrm{C}
\end{aligned}
\end{aligned}
$$

where $p$ is in atm. The standard deviation in pressure for these equations, in the range of present measurements, is $0.08 \%$; the maximum deviation is $0.20 \%$.

For benzene, present measured vapor pressures agree with those of Bender (1) within $0.08 \%$ on the average and $0.15 \%$ at the maximum. For $n$-octane, the authors measured values agree with those of Young (11) within $0.7 \%$ on the average and $1.1 \%$ at the maximum. Our measured critical constants are $288.84^{\circ} \mathrm{C}$. and 48.28 atm . for benzene, and $295.62^{\circ} \mathrm{C}$. and 24.55 atm . for $n$-octane.

## SATURATED VAPOR AND SATURATED LIQUID VOLUMES

The volumes of the vapor at its saturation points were obtained by detecting the discontinuity in the pressurevolume isotherms of the gas phase. They are listed in Table I.
Saturated liquid volumes were obtained by visually noting the volume at which the last trace of vapor disappeared upon an increase in pressure of 0.01 atm . The results

## Table I. Saturated Vapor Volumes

| Temp. ${ }^{\circ}$ C. | Benzene, <br> L./Mole | $n$-Octane, <br> L./Mole |
| :---: | :---: | :---: |
| 160 | 4.388 | $\ldots$ |
| 170 | 3.635 | $\ldots$ |
| 180 | 3.035 | 7.115 |
| 190 | 2.539 | 5.834 |
| 200 | 2.136 | 4.806 |
| 210 | 1.798 | 3.970 |
| 220 | 1.517 | 3.284 |
| 230 | 1.282 | 2.716 |
| 240 | 1.078 | 2.242 |
| 250 | 0.903 | 1.834 |
| 260 | 0.747 | 1.482 |
| 270 | 0.606 | 1.168 |
| 280 | 0.473 |  |

were represented, with a standard deviation of $0.06 \%$ and a maximum deviation of $0.15^{-} \mathrm{r}$, by the equations:

Benzene, $130^{\circ} \leqq t \leqq 280^{\circ} \mathrm{C}$.
$\log v_{0}=0.10117+0.84465 x-3.3522 x^{2}+$
$10.0208 x^{3}-14.7420 x^{4}+8.7872 x^{5}$
$n$-Octane, $190^{\circ} \leqq t \leqq 280^{\circ} \mathrm{C}$.

$$
\log v_{0}=0.21338+0.46260 x-0.57736 x^{2}+0.59972 x^{3}
$$

where

$$
x=10^{-10} t^{4}, \text { and } v_{0} \text { is in cubic centimeters per gram }
$$

## LIQUID COMPRESSIBILITIES

For each pressure-volume isotherm, the observed liquid specific volumes were fitted to equations of the form:

$$
\begin{equation*}
v=a+b p^{-1}+c p+d p^{2}+e p^{3} \tag{1}
\end{equation*}
$$

where $v$ is in cubic centimeters per gram and $p$ is not greater than 180 atm . The constants for this equation and the standard deviations are given in Table II.

The benzene isotherms at $237.78^{\circ} \mathrm{C}$. and the $n$-octane isotherm at $275^{\circ} \mathrm{C}$. were measured to obtain direct comparisons with the highest temperature measurements of Glanville (5) and Felsing (3). At $237.78^{\circ}$ C., the authors specific volumes for benzene lie $0.9 \%$ above Glanville's. At $275^{\circ} \mathrm{C}$. present $20-\mathrm{atm}$. specific volumes for $n$-octane are $0.1 \%$ smaller than those of Felsing and the authors $150-\mathrm{atm}$. specific volumes are $0.4 \%$ larger.

## heats of vaporization

The heats of vaporization of liquid benzene and $n$-octane were derived by the Clapeyron equation from the saturated vapor and saturated liquid volumes and the slopes of the vapor pressure curves. These derived heats were combined with calorimetric values, measured at lower temperatures (4, 7-10) and fitted by least squares to obtain the following equations (Griffith's values were taken from the equation of Sutcliffe (4). A.P.I. Project 44 values and the value of zero at the critical point were each given a weight of 5 in the least-squares procedure.)

## Benzene,

$$
\begin{equation*}
\Delta H_{v}=46.25+178.38 \mathrm{y}-201.8 \mathrm{y}^{3}+224 \mathrm{y}^{4} \tag{2}
\end{equation*}
$$

$n$-Octane,

$$
\begin{equation*}
\Delta H_{v}=38.61+146.03 y-142.5 y^{3}+169 y^{4} \tag{3}
\end{equation*}
$$

$\Delta H_{v}$ is in calories per gram ( $1 \mathrm{cal} .=4.1840$ absolute joules) and

$$
y=\left[\left(\log \frac{T_{c}}{T}\right)^{1 / 3}-0.3\right]
$$

where $T_{c}$ is the critical temperature from this work in ${ }^{\circ} \mathrm{K}$. ( $T_{0}=273.16^{\circ} \mathrm{K}$ ). These equations are valid from $25^{\circ} \mathrm{C}$. to the critical temperature. The standard deviation from the experimental values is 0.09 cal . per gram for benzene and 0.18 cal. per gram for $n$-octane. The deviations are plotted in Figure 1, where the zero line represents zero deviation from Equations 2 and 3 .

Table II. Liquid Compressibilities, Constants For Equation I

| $t,{ }^{\circ} \mathrm{C}$ | $a$ | $b$ | $c \times 10^{2}$ | $d \times 10^{4}$ | $e \times 10^{6}$ | Std. Dev., \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Benzene |  |  |  |  |  |  |
| 130 | 1.3259 | -0.0008 | -0.03389 | 0.00321 | 0 | 0.03 |
| 140 | 1.3488 | 0.0010 | -0.03923 | 0.00439 | 0 | 0.03 |
| 150 | 1.3733 | 0.0039 | -0.04374 | 0.00512 | 0 | 0.03 |
| 160 | 1.3992 | 0.0065 | -0.04956 | 0.00583 | 0 | 0.04 |
| 170 | 1.4276 | 0.0161 | -0.05737 | 0.00724 | 0 | 0.03 |
| 180 | 1.4578 | 0.0318 | -0.06522 | 0.00831 | 0 | 0.04 |
| 190 | 1.4907 | 0.0517 | -0.07563 | 0.01028 | 0 | 0.04 |
| 200 | 1.5275 | 0.1062 | -0.09061 | 0.01409 | 0 | 0.04 |
| 210 | 1.5659 | 0.2134 | -0.10350 | 0.01637 | 0 | 0.05 |
| 220 | 1.6106 | 0.3840 | -0.12189 | 0.01971 | 0 | 0.05 |
| 230 | 1.6589 | 0.7126 | -0.14717 | 0.02645 | 0 | 0.05 |
| 237.78 | 1.6926 | 1.2474 | -0.16040 | 0.02838 | 0 | 0.05 |
| 240 | 1.7019 | 1.4461 | -0.16528 | 0.02942 | 0 | 0.05 |
| 250 | 1.7387 | 3.0596 | -0.18012 | 0.03309 | 0 | 0.05 |
| 260 | 1.7185 | 7.1868 | -0.14370 | 0.02105 | 0 | 0.02 |
| 270 | 1.5578 | 17.2990 | +0.00666 | -0.02080 | 0 | 0.16 |
| $n$-Octane |  |  |  |  |  |  |
| 130 | 1.6471 | 0 | -0.05551 | 0.00684 | 0 | 0.00 |
| 150 | 1.7040 | 0 | -0.07070 | 0.00944 | 0 | 0.03 |
| 170 | 1.7674 | 0 | -0.09147 | 0.01377 | 0 | 0.03 |
| 190 | 1.8472 | 0.0027 | -0.14396 | 0.04913 | -0.00983 | 0.02 |
| 200 | 1.8910 | 0.0123 | -0.16541 | 0.05538 | -0.01015 | 0.02 |
| 210 | 1.9435 | 0.0288 | -0.20228 | 0.07360 | -0.01351 | 0.02 |
| 220 | 1.9931 | 0.0761 | -0.23736 | 0.09200 | -0.01787 | 0.03 |
| 230 | 2.0551 | 0.1539 | -0.29022 | 0.12135 | -0.02402 | 0.03 |
| 240 | 2.1194 | 0.3415 | -0.34655 | 0.15275 | -0.03099 | 0.04 |
| 250 | 2.1899 | 0.7176 | -0.41331 | 0.19155 | -0.03985 | 0.04 |
| 260 | 2.2426 | 1.7529 | -0.44795 | 0.20452 | -0.04153 | 0.04 |
| 270 | 2.2334 | 4.4497 | -0.38120 | 0.14705 | -0.02605 | 0.03 |
| 275 | 2.1725 | 7.1605 | -0.25548 | 0.05582 | -0.00359 | 0.04 |
| 280 | 2.0119 | 11.9890 | +0.03379 | -0.14164 | +0.04268 | 0.12 |



Figure 1. Comparison of Equations 2 and 3 with experiment

## LITERATURE CITED

(1) Bender, P. Furukawa, G.T., Hyndman, J.R., Ind. Eng. Chem. 44, 387 (1952).
(2) Connolly, J.F., Kandalic, G.A., Phys. Fluids 3, 463 (1960).
(3) Felsing, W.A., Watson, G.M., J. Am. Chem. Soc. 64, 1822 (1942).
(4) Fiock, E.F., Ginnings, D.C., Holton, W.B., J. Research Natl. Bur. Standards 6, 899 (1931).
(5) Glanville, J.W., Sage, B.H., Ind. Eng. Chem. 41, 1272 (1949).
(6) Gornowski, E.J., Amick, E.H., Jr., Hixon, A.N., Ind. Eng. Chem. 39, 1348 (1947).
(7) Griffiths, E.H., Marshall, D., Phil. Mag. 41, 1 (1896).
(8) McKay, R.A., Sage, B.H., J. Chem. Eng. Data 5, 21 (1960).
(9) Rossini, F.D., Pitzer, K.S., Arnett, R.L., Braun, R.M., Pimentel, G.C., "Selected Values of Physical and Thermodynamic Properties of Hydrocarbons and Related Compounds," Carnegie Press, Pittsburgh, 1953.
(10) Sutcliffe, J.A., Lay, F.C., Prichard, W.L., Proc. Roy. Soc. London A 115, 88 (1927).
(11) Young, S., Sci. Proc. Roy. Dublin Soc. 12, 374 (1910).

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